



BEAM DESIGN CACULATION- B1



Data-Beam B1

Material C40/50,	$f_{ck} := 40 \frac{N}{mm^2}$	$f_y := 460 \frac{N}{mm^2}$
$b_w := 150mm$	$D := 450mm$	$d_c := 25mm$
Span of beam,		$L := 2.57m$

Floor Finish (Stone Finish, 50Bed, Ceiling), $W_{ff} := \left[(0.5 + 1 + 0.15) \frac{kN}{m^2} \right]$

Unit weight of concrete, $\gamma := 25 \frac{kN}{m^3}$

Live load on Slab $W_f := 1.5 \frac{kN}{m^2}$

Thickness of Ground Floor Slab, $D_{slab} := 225mm$

Total load of internal block wall, $W_{bw} := 3.45 \frac{kN}{m^2}$

Height of internal block wall, $H_{bw} := 3.005m$

Load calculations on Beam B1

Ultimate Load from block wall, (due to selfweight) $UL_{wall} := 1.35(H_{bw} \cdot W_{bw})$ $UL_{wall} = 14 \cdot \frac{kN}{m}$

Contributory span of slab, for beam $Span := \frac{2.56m}{2} + 0.8m$ $Span = 2.08m$

Dead Load from GF slab, (DL) $DL_f := D_{slab} \cdot \gamma \cdot Span + W_{ff} \cdot Span$ $DL_f = 15.132 \cdot \frac{kN}{m}$

Live Load from GF slab, (LL) $LL_f := W_f \cdot Span$ $LL_f = 3.12 \cdot \frac{kN}{m}$

Ultimate Load from GF slab, (due to DL & LL) $UL_{slab} := 1.35 \cdot (DL_f) + 1.5(LL_f)$ $UL_{slab} = 25.108 \cdot \frac{kN}{m}$

Ultimate Load from beam, (due to selfweight) $UL_{beam} := 1.35 \cdot (b_w \cdot D \cdot \gamma)$ $UL_{beam} = 2.3 \cdot \frac{kN}{m}$

Ultimate Load on beam, (due to slab & wall above) $UL_{total} := UL_{wall} + UL_{slab} + UL_{beam}$ $UL_{total} = 41.4 \cdot \frac{kN}{m}$

Maximum moment, $M_u := \frac{UL_{total} \cdot L^2}{8}$ $M_u = 34.2 \cdot kN \cdot m$

Maximum shear, $Q_u := \frac{UL_{total} \cdot L}{2}$ $Q_u = 53.2 \cdot kN$



Flexure Reinforcement

$$d := D - d_c \quad d = 425 \cdot \text{mm} \quad d1 := d - d_c \quad d1 = 400 \cdot \text{mm}$$

$$\text{Limiting Moment,} \quad M_{ulim} := 0.167 \cdot f_{ck} \cdot b_w \cdot d^2 \quad M_{ulim} = 181 \cdot \text{kN} \cdot \text{m}$$

$$M_{comp} := \max[(M_u - M_{ulim}), 0] \quad M_{comp} = 0 \cdot \text{kN} \cdot \text{m}$$

$M_u < M_{ulim}$ so compression reinforcement is not required

$$\text{Compression reinforcement,} \quad A_{sc} := \frac{M_{comp}}{0.87 f_y \cdot d1} \quad A_{sc} = 0 \cdot \text{mm}^2$$

Tension reinforcement,

$$M_{des} := \min(M_u, M_{ulim}) \quad M_{des} = 34.2 \cdot \text{kN} \cdot \text{m}$$

$$k := \frac{M_{des}}{b_w \cdot d^2 \cdot f_{ck}} \quad k = 0.032$$

$$\text{Lever arm} \quad l_a := 0.5 + \sqrt{0.25 - \frac{k}{0.908}} \quad l_a = 0.964$$

$$l_{amax} := \text{if}(l_a < 0.95, l_a, 0.95)$$

$$A_{st} := \left(\frac{M_{des}}{l_{amax} \cdot d \cdot 0.87 \cdot f_y} \right) + A_{sc} \quad A_{st} = 211.4 \cdot \text{mm}^2$$

Provide n := 2 nos ϕ := 16mm dia

$$A_{s1} := n \cdot \frac{\pi \cdot \phi^2}{4} \quad A_{s1} = 402.124 \cdot \text{mm}^2$$

Shear Reinforcement

$$\text{Flexural Reinforcement} \quad A_{s1} = 402.124 \cdot \text{mm}^2$$

$$\rho := \text{if} \left(\frac{A_{s1}}{b_w \cdot d} \leq 0.02, \frac{A_{s1}}{b_w \cdot d}, 0.02 \right) \quad \rho = 6.308 \times 10^{-3}$$

$$v := 0.699 - \frac{f_{ck} \cdot \frac{\text{mm}^2}{\text{N}}}{200}$$

$$v = 0.499$$

$$v := \text{if}(v < 0.5, 0.5, v)$$

$$v_{max} := 0.3 \cdot v \cdot f_{ck}$$

$$v_{max} = 6 \cdot \frac{\text{N}}{\text{mm}^2}$$



$$v_c = 0.689 \cdot \frac{N}{\text{mm}^2}$$

$$V_{Rd2} := v_{\max} \cdot b_w \cdot d \quad V_{Rd2} = 382.5 \cdot \text{kN}$$

$$V_{Rd3} := Q_u$$

Applied shear stress $v := \frac{V_{Rd3}}{b_w \cdot d} \quad v = 0.834 \cdot \frac{N}{\text{mm}^2}$ (Shear reinforcement to be provided)

Assuming stirrups dia, $\phi_1 := 8\text{mm}$ at spacing, $s := 250\text{mm}$

$$A_{sw.req} := 1.28(v - v_c) \cdot \frac{b_w \cdot s}{f_y} \quad A_{sw.req} = 15.136 \cdot \text{mm}^2$$

$$A_{swprov} := 2 \cdot \frac{\pi \cdot \phi_1^2}{4} \quad A_{swprov} = 100.531 \cdot \text{mm}^2$$